

**LABORATORY MEASUREMENT OF
THE REDUCTION OF
TRANSMITTED IMPACT SOUND OF
OAK LAMINATE ON SILENT
SHIELD UNDERLAY
(ACCORDING TO ISO 10140-3)**

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Date: 13th November 2017



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**LABORATORY MEASUREMENT OF THE
REDUCTION OF TRANSMITTED IMPACT
SOUND BY FLOOR COVERINGS ON A
STANDARD FLOOR.**

(According to ISO 10140-3)

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Reduction of impact sound pressure level according to ISO 10140-3
Laboratory measurements of the reduction of transmitted impact sound by floor coverings on a heavyweight reference floor

Client: Jacobsen Creative Surface

Date of test: 25 October 2017

Test rooms: Reverberation Chambers A and B

Description and identification of the test specimen and test arrangement: -

A 3.2 m x 3.2 m sample of *14 mm UNICLIC Oak timber laminate flooring* (14 mm x 190 mm x 1820 mm planks)
 Loose laid
 1 layer of *Silent Shield underlay*
 Loose laid
 Concrete Slab

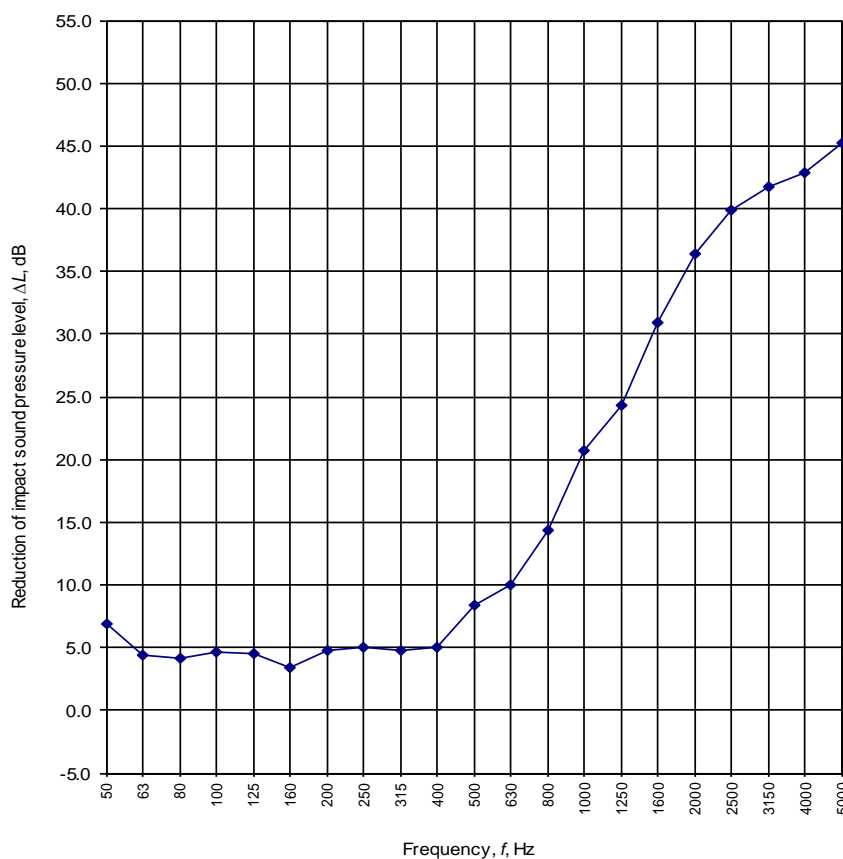
Source chamber was Chamber A and receiving chamber was Chamber B. Test specimen installed by the client. Curing times: 125 (72hrs). Grout (24hrs)
 Deviation from standard: The bare test floor used is of uniform thickness for an area of only 2.6m x 2.6m. The description of the bare test floor is given in the full report.

Air temp in the test rooms: 19 °C

Air humidity in test rooms: 52 %

Receiving room volume: 153 m³

Frequency <i>f</i> Hz	$L_{n,0}$ One-third octave dB	ΔL One-third octave dB
50	54.4	6.9
63	50.0	4.4
80	56.8	4.2
100	63.7	4.7
125	65.8	4.5
160	66.1	3.4
200	68.7	4.8
250	72.1	5.0
315	71.3	4.8
400	69.9	5.0
500	74.2	8.4
630	72.0	10.0
800	71.2	14.3
1000	71.3	20.7
1250	71.3	24.3
1600	71.1	30.9
2000	72.0	36.4
2500	72.5	39.9
3150	72.6	41.7
4000	71.1	42.9
5000	68.2	45.2



Notes: #N/A = Value not available. **Bold** values are used to calculate ΔL_w .

< indicates that the true value is lower.

$L_{n,0}$ are the bare floor impact sound levels.

Rating according to ISO 717-2:

 $\Delta L_w = 19$ dB $C_{i,\Delta} = 10$ dB $C_{i,r} = -1$ dB $C_{i,150-2500} = -1$ dB

These results are based on a test made with an artificial source under laboratory conditions (engineering Method) with the specified reference floor.

No. of test report: **T1741-5**

Name of test institute: University of Auckland Acoustics Testing Service.

Date: 13-November-2017

Signature: 

ANNEX A.

PHOTOS OF TEST SPECIMEN IN CHAMBER.



Figure 1: Oak Flooring



Figure 2: Section view of flooring



Figure 3: Oak flooring on Silent Shield underlay

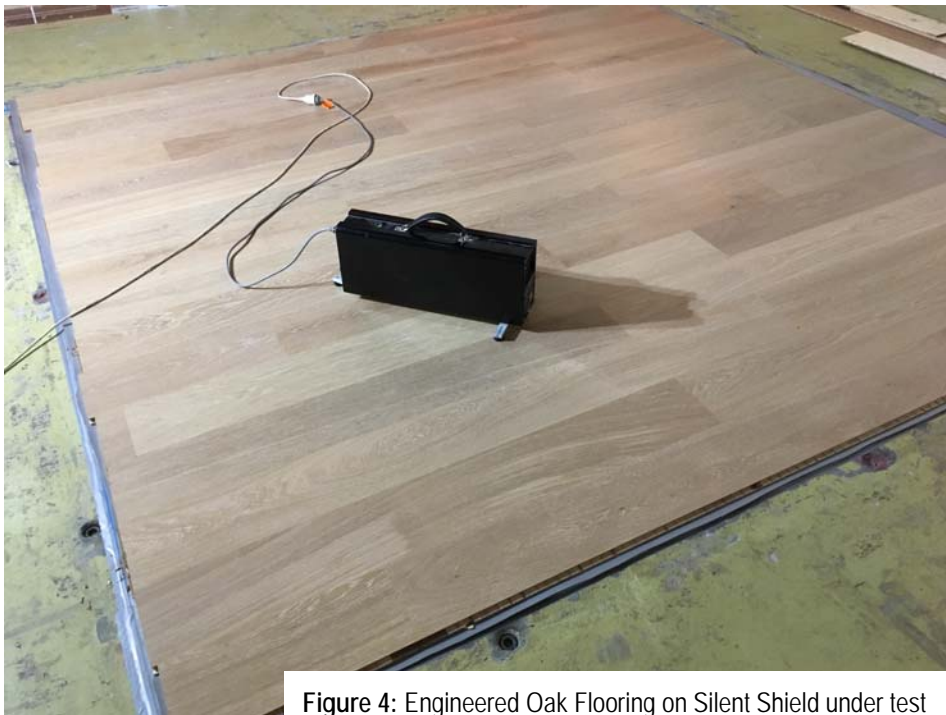


Figure 4: Engineered Oak Flooring on Silent Shield under test



ADDITIONAL INFORMATION ABOUT EQUIPMENT USED.

INSTRUMENTATION	EQUIPMENT	TYPE / SERIAL No.
CHAMBER A SOURCE ROOM		
	1/2" Microphone	4190/2150379
	Preamplifier	2619 / 945952
	Rotating Boom	3923 / 936496
	Tapping Machine	EM50/F3.090142
CHAMBER B RECEIVING ROOM		
	1/2" Microphone	4165 / 1622303
	Preamplifier	2619 / 945949
	Rotating Boom	3923 / 936497
Calibration of the above equipment was conducted by Electroacoustic Calibration Services (ECS), an IANZ registered laboratory.		
BOTH ROOMS		
	Pistonphone	4231 / 2241899
	Analyzer	01dB Stell / 01381



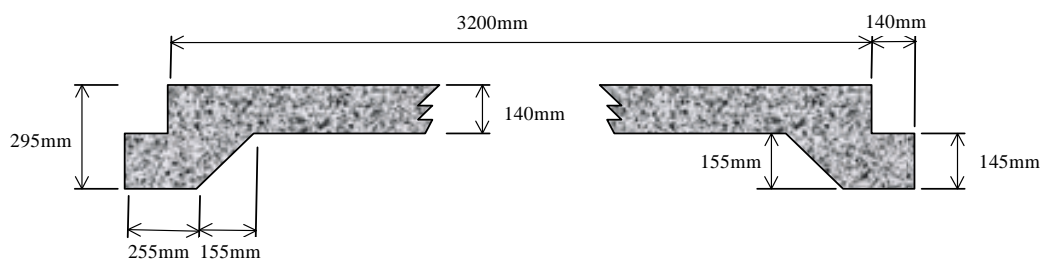
ANNEX C.

SUMMARY OF THE MEASUREMENT OF IMPACT SOUND INSULATION OF FLOORS.

INSTALLATION OF TEST SAMPLE

The floor/ceiling system under test is installed in the opening between the two large reverberation chambers – chambers B and A. These chambers are vibration isolated from each other which results in a structural discontinuity at the middle of the test opening. This gap is covered over by a wooden collar, which seals the gap and provides for ease of fixing of samples

The sample is constructed by the client following the techniques normally used in practice for that type of floor/ceiling system, and is sealed into the test opening with perimeter seals of acoustic sealant.



METHOD

The normalized impact sound pressure levels are obtained in accordance with the recommendations of ISO standard 10140-3 "Measurements of impact sound insulation."

The BK3204 tapping machine is placed sequentially in four different positions on the floor. The impact sound pressure level is measured in the room below the floor, using a rotating microphone, in third octave frequency bands. The impact sound pressure levels are normalized against the room absorption. The room absorption is calculated from the reverberation time and room volume. The reverberation time is measured from the decay of a steady state sound field.

Corrections are applied, where necessary, for airborne sound transmission and background noise. The airborne sound transmission is determined using a loudspeaker and the microphone.

RESULTS

The third octave band normalized impact sound pressure levels L_n are presented in both table and graph formats. Sometimes a highly reflective test sample means that the lower frequency normalized impact sound pressure levels cannot be reliably measured; this is indicated by #N/A in the table of results. Additionally, sometimes the airborne transmission of sound through the floor or loud background noise affects the measurements resulting in only an upper threshold being found; this is indicated by a < sign preceding the tabulated results.

Single figure ratings are also presented. The weighted normalized impact sound pressure level $L_{n,w}$, determined according to ISO 717-2, is presented along with a spectrum adaptation term G_1 . $L_{n,w}$ is determined by fitting a reference curve to the third octave band normalized impact sound pressure levels L_n from 100Hz to 3150Hz, and gives a single figure determination of the sound levels which are transmitted through the floor from impacts (higher is worse). The spectrum adaptation term G_1 is used to suggest the presence of high level peaks in the results over the frequency range 100Hz to 2500Hz, and may be added to $L_{n,w}$. For massive floors with effective coverings G_1 will be about zero, for light timber floors G_1 will be slightly positive, and for concrete floors with less effective covering G_1 will range from -15 dB to 0dB. Another spectrum adaptation term $G_{1,50-2500}$, which covers the frequency range from 50Hz to 2500Hz, may also be presented if the low frequency levels are available.

The impact insulation class (IIC) determined according ASTM E989 is also presented. This is determined by fitting a reference curve to the third octave band normalized impact sound pressure levels L_n from 100Hz to 3150Hz, but in a slightly different way to ISO 717-2. The impact insulation class measures the insulating abilities of the floor so that higher is better (contrary to $L_{n,w}$).



ANNEX D.

DESCRIPTION OF REVERBERATION CHAMBERS AT THE ACOUSTICS RESEARCH CENTRE

There are three large interconnected reverberation chambers at the Acoustics Research Centre, two at ground level (Chambers C and A) and the third (Chamber B) below A.

All three reverberation chambers may be described as hexagonal prisms; each having 6 vertical sided walls, perpendicular to the floor. The roofs of chamber A and C are plane, but inclined at 12 degrees from horizontal. Chamber B has a plane, horizontal roof which is the floor of chamber A above it. The floor of chamber B is also horizontal, but has two angled sections at its north west and south east ends. The centre section is horizontal because a floor jack is installed there. The floor jack may be raised hydraulically to the ceiling of chamber B, the centre of which consists of a floor plug between the two chambers. This plug may be disconnected from chamber A and lowered down into chamber B, leaving a 3.2m x 3.2 m opening between the two chambers. This allows for the measurement of airborne and impact insulation of floor and roof elements.

The wall of chamber C adjacent to chamber A is left open, and the corresponding wall of chamber A consists of a pair of iron doors that are clamped against the chamber. The clamps may be removed and the iron doors pulled back, leaving the entire wall area (4.6m wide x 2.74m high) between the chambers open. This allows for the measurement of airborne sound insulation of wall elements.

Chamber A has a rotating vane diffuser in a central position with an area (both sides) of about 53 m². It has the shape of two cones with their bases joined, with the two opposite quadrants of one cone open and the complementary quadrants in the other cone open. Chamber C has a similar rotating vane diffuser but it is smaller, having a total area of about 27 m².

In addition, up to ten static diffusers may be employed if needed. These are constructed of two laminated layers of dense Formica, of dimensions 2m x 2m. The Formica elements are riveted to a frame constructed of aluminium T section. Four aluminium arms may be bolted onto the frame to allow the diffusers to be mounted as desired.

Currently two of these are used in chamber C, and three are used in chamber B.

The volumes and surface areas of the reverberation chambers are as follows:

	VOLUME (m ³)	SURFACE AREA (m ²)
Chamber A	202 ± 3	203.6 ± 0.9
Chamber B	153 ± 2	173 ± 1
Chamber C	209 ± 4	214 ± 0.9

The three Reverberation Chambers are linked by heavy steel doors and a removable Standard Industrial Floor Section which is removed and repositioned by a hydraulic hoist. The three chambers are vibration isolated from one another so that sound can only pass from one to the other via the intervening Test Wall or Test Floor/Ceiling

